ECE 463/663 - Homework #13

VSS & Saturating Control. Due Monday, May 5th

VSS Control

1) For the cart and pendulum system of homework set #4:

$$s\begin{bmatrix} x\\ \theta\\ \dot{x}\\ \dot{\theta}\\ \dot{\theta}\end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 & 0\\ 0 & 0 & 0 & 1\\ 0 & -19.6 & 0 & 0\\ 0 & 19.6 & 0 & 0 \end{bmatrix} \begin{bmatrix} x\\ \theta\\ \dot{x}\\ \dot{\theta}\end{bmatrix} + \begin{bmatrix} 0\\ 0\\ 0.667\\ -0.444 \end{bmatrix} F$$

(x2, y2) m2 = 3kg L = 1.5m X F (x1,y1) m1 = 1.5kg

Design a VSS control law so that the cart and pendulum system behaves like the following reference model:

```
\boldsymbol{y}_m = \left(\frac{4}{(s+2)\left(s^2+s+2\right)}\right)\boldsymbol{R}
A = [0, 0, 1, 0; 0, 0, 0, 1; 0, -19.6, 0, 0; 0, 19.6, 0, 0];
B = [0;0;0.6667; -0.4444];
C = [1, 0, 0, 0];
N = length(A);
T1 = [];
for i=1:N
   T1 = [T1, (A^{(i-1))*B];
end
P = poly(eig(A));
T2 = [];
for i=1:N
    T2 = [T2; zeros(1,i-1), P(1:N-i+1)];
end
T3 = zeros(N, N);
for i=1:N
     T3(i, N+1-i) = 1;
end
T = T1*T2*T3;
>> conv([2,1],[2,1,1])
ans = 4 4 3
                                 1
>> Kx = [4, 4, 3, 1] * inv(T)
Kx = -0.9180 - 8.1280
                                -0.9180 -3.6275
>> eig(A - B*Kx*100)
```

ans = -97.1559 -0.4995 + 1.4078i -0.4995 - 1.4078i -1.8451

Another way to see this, the zeros of the transfer funciton from F to the sliding surface should be the desired pole locations

Check: the zeros are the desired closed-loop poles.

Note that the closed-loop poles go to the zeros as the feedback gain goes to infinity:

```
>> eig(A - B*Kx)
   -4.6859
                           gain of one doesn't work: A - B*Kx*1 is unstable
   3.4162
   -0.3829
    0.6526
>> eig(A - B*Kx*10)
  -9.2943
                           still unstable with a gain of 10
   0.1625 + 2.0370i
   0.1625 - 2.0370i
  -1.0307
>> eig(A - B*Kx*100)
 -97.1559
                           close - feedback gain of 100 drives poles to zeros
  -0.4995 + 1.4078i
  -0.4995 - 1.4078i
  -1.8451
>> eig(A - B*Kx*1000)
  -997.01
                           closer - feedback gain of 1000 drives closer
  -0.5005 + 1.3309i
  -0.5005 - 1.3309i
  -1.9844
```

2) Find the step response of your control law on the linear model

```
Kx = [-0.9180 -8.1280 -0.9180 -3.6275];
while(t < 29)
    Ref = sign(sin(t*2*pi/30);
    U = -10 * sign(Kx * (X - [Ref;0;0;0]));
    dX = A*X + B*U;
    X = X + dX * dt;
    t = t + dt;
    y = [y ; X(1), Ref, U];
    end
```





3) Find the step respone of your control law on the nonlinear simulation

```
Kx = [-0.9180 -8.1280 -0.9180 -3.6275];
while(t < 29)
    Ref = 1*(sin(t*2*pi/30) > 0);
    U = -10 * sign(Kx * (X - [Ref;0;0;0]));
    dX = CartDynamics(X, U);
    X = X + dX * dt;
    t = t + dt;
    n = mod(n+1, 50);
    if(n == 0)
        CartDisplay(X, X, Ref);
        end
    y = [y ; X(1), Ref, U];
    end
```



Nonlinear Simulation for a VSS controller



Position (x) for a VSS controller



Input (U) for a VSS controller

Saturating Control:

4) Design a saturating control law so that the cart and pendulum system behaves like the following reference model:

$$\mathbf{y}_m = \left(\frac{4}{(s+2)\left(s^2+s+2\right)}\right)\mathbf{R}$$

Same as before but change U

$$U = -10 \cdot sign(CX)$$

to

 $U = -10 \cdot \text{limit}(CX)$

where *limit()* is a saturation funciton

limit(x)=
$$\begin{cases} +1 & x > 1 \\ x & -1 < x < 1 \\ -1 & x < -1 \end{cases}$$

and C places the zeros

C = Kx = [-0.9180 - 8.1280 - 0.9180 - 3.6275]

(same as before)

5) Find the step response of your control law on the linear model

Change one line of code:

```
% VSS
% U = -10 * sign(Kx * (X - [Ref;0;0;0]));
% Saturating
U = -100 * (Kx * (X - [Ref;0;0;0]));
U = max(-10, min(10, U));
```



Position for a saturating controller



Input (U) for a saturating controller



6) Find the step respone of your control law on the nonlinear simulation

Output for a Saturating Controller & Nonlinear Simulation



Position (x) for a Saturating Controller (almost identical to a VSS controller)



Input (U) for a Saturating Controller