## ECE 463/663 - Homework #12

LQG/LTR. Due Monday, April 28th

## LQG / LTR

For the cart and pendulum system of homework set #4:

$$s\begin{bmatrix} x \\ \theta \\ \dot{x} \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & -19.6 & 0 & 0 \\ 0 & 19.6 & 0 & 0 \end{bmatrix} \begin{bmatrix} x \\ \theta \\ \dot{x} \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0.667 \\ -0.444 \end{bmatrix} F$$

Design a control law so that the cart and pendulum system behaves like the following reference model:

$$\mathbf{y}_m = \left(\frac{2}{s^2 + s + 2}\right) \mathbf{R}$$

LQG/LTR without a Servo Compensator:

1) Give a block diagram for your controller





2) (20pt) Plot the step response of the model and the linearlized plant for yor control law for

- $Q = 100 e^2$
- $Q = 1,000 e^2$
- $Q = 10,000 e^2$

Q = 100 e<sup>2</sup> Kx = -10.0000 -154.5162 -15.0076 -47.5723 Km = 3.1606 0.3732





Model (green) & Plant (blue)

Q = 1000 e^2 Kx = -31.6228 -246.4828 -36.1315 -84.1349 Km = 14.0914 9.2704



Model (green) & Plant (blue)

Q = 10,000 e^2 Kx = -100.0000 -503.5900 -96.8145 -185.1335 Km = 47.3710 46.1804





## Code

```
A = [0, 0, 1, 0; 0, 0, 0, 1; 0, -19.6, 0, 0; 0, 19.6, 0, 0];
B = [0;0;0.6667;-0.4444];
C = [1, 0, 0, 0];
Ref = 1;
dt = 0.01;
t = 0;
%Reference Model
Gm = tf(2, [1, 1, 2]);
Gss = ss(Gm);
Am = Gss.A;
Bm = Gss.B;
Cm = Gss.C;
Dm = Gss.D;
[n,m] = size(Am);
A6 = [A, zeros(4, n);
       zeros(n,4), Am];
B6 = [B; zeros(n,1)];
B6r = [zeros(4,1); Bm];
C6 = [C, -Cm];
Q = C6' * C6;
R = 1;
K6 = lqr(A6, B6, Q*1e4, 1);
Kx = K6(1:4);
Km = K6(5:4+n);
X = zeros(4, 1);
Xm = zeros(n, 1);
n = 0;
y = [];
while(t < 29)
    Ref = 1*(sin(0.2*t) > 0);
    U = -Km * Xm - Kx * X;
    dX = CartDynamics(X, U);
    dXm = Am*Xm + Bm*Ref;
    X = X + dX * dt;
    Xm = Xm + dXm * dt;
    t = t + dt;
    n = mod(n+1, 5);
    if(n == 0)
       CartDisplay(X, [Cm*Xm;0;0;0], Ref);
       end
    y = [y ; X(1), Cm*Xm, Ref];
    end
hold off;
t = [1:length(y)]' * dt;
plot(t,y);
```

## LQG/LTR with a Servo Compensator:

3) Give a block diagram for your controller plus servo compensator



$$s\begin{bmatrix} X\\ Z\\ X_m \end{bmatrix} = \begin{bmatrix} A & 0 & 0\\ C & 0 & -C_m\\ 0 & 0 & A_m \end{bmatrix} \begin{bmatrix} X\\ Z\\ X_m \end{bmatrix} + \begin{bmatrix} B\\ 0\\ 0 \end{bmatrix} U + \begin{bmatrix} 0\\ 0\\ B_m \end{bmatrix} R$$
$$U = \begin{bmatrix} -K_x & -K_z & -K_m\\ \end{bmatrix} \begin{bmatrix} X\\ Z\\ X_m \end{bmatrix}$$

4) (20pt) Plot the step response of the model and the linearlized plant for yor control law for

- $Q = 100 z^2$
- $Q = 1,000 z^2$
- $Q = 10,000 z^2$

Q = 100 z^2 Kx = -20.6909 -180.7282 -21.4056 -58.0681 Kz = -10.0000 Km = 5.9343 7.0263





Model (green) & Plant (blue)

```
Q = 1000 z^2
Kx = -51.0518 -263.4277 -41.2091 -90.8204
Kz = -31.6228
Km = 16.9527 26.0676
```



Model (green) & Plant (blue)

Q = 10,000 z^2 Kx = -132.1594 -451.6872 -87.3305 -164.7866 Kz = -100.0000 Km = 43.2913 84.2529



Model (green) & Plant (blue)

Sidelight: Part of the problem is you're trying to make a 4th-order system behave like a 2nd-order system. It works a little better if you make the reference model 4th-order as well:





Kx = -132.1594 -451.6872 -87.3305 -164.7866 Km = -100.0000 162.3067 144.8585 41.9802 10.5377

It works a little better if you add a right-half plane zero to create undershoot

• A reference model that takes into account how the plant *wants* to behave tends to work better than a reference model that ignores the plant's dynamics.

$$\mathbf{G}_m = \left(\frac{-2(s-3)}{(s+1.5)(s+2)(s^2+s+2)}\right)$$

