## Control of a RR Robot

Consider the problem of controlling the tip-position of a 2-link robotic arm. Assume it is to trace out a square:


From before, the dynamics of the robotic arm are:

$$
\left[\begin{array}{cc}
\left(4+2 c_{2}\right) & \left(1+c_{2}\right) \\
\left(1+c_{2}\right) & 1
\end{array}\right]\left[\begin{array}{l}
\ddot{\theta}_{1} \\
\ddot{\theta}_{2}
\end{array}\right]=\left[\begin{array}{c}
T_{1} \\
T_{2}
\end{array}\right]+\left[\begin{array}{c}
2 \mathrm{~s}_{2} \dot{\theta}_{1} \dot{\theta}_{2}+\mathrm{s}_{2} \dot{\theta}_{2}^{2} \\
-\mathrm{s}_{2} \dot{\theta}_{1}^{2}
\end{array}\right]+\mathrm{g}\left[\begin{array}{c}
3 \mathrm{c}_{1}+\mathrm{c}_{12} \\
\mathrm{c}_{12}
\end{array}\right]
$$

To control the angle of each motor, you need to

- Define the desired angle at any given time (the set-point), and
- Determine the torque required to drive the motor to that angle.

First, let's use the previous path-planning routines for the RRR robot to define the desired

- Tip positions, and
- Joint angles

First, define the tip positions. Using the MoveTo() routine from before, this can be done as follows:

```
disp('Defining Path to Follow');
P1 = [0.5, 0]';
P2 = [1.5, 0]';
P3 = [1.5,-1]';
P4 = [0.5,-1]';
P5 = P1;
disp('Calculating tip positions');
% Determine the tip positions every 10ms
[A,T1] = MoveTo(P1,P2,2);
[A,T2] = MoveTo(P2,P3,2);
[A,T3] = MoveTo(P3,P4,2);
[A,T4] = MoveTo(P4,P5,2);
TIP = [T1,T2,T3,T4];
```



## Desired Tip Position to Trace Out a Square

Next, convert these to joint angles. To do this, write a routine to compute the joint angle given the tip position:

```
function [Q] = InverseRR(TIP)
x = TIP(1);
y = TIP(2);
r = sqrt(x^2 + y^2);
Qa = atan2(y, x);
Qb = acos(r/2);
Q1 = Qa - Qb;
Q2 = 2*Qb;
Q = [Q1; Q2];
end
```

With this, convert tip positions to joint angles

```
disp('Calculating joint angles');
% Determie the joint angles every 10ms
Qr = [];
for i=1:length(TIP)
    q = InverseRR(TIP(:,i));
    Qr = [Qr, q];
end
```



Desired Joint Angles vs Time for tracing out a square

Once you know where the joint angles are supposed to be, you can start definining the feedback control law.

## PD Control

If you have decoupled systems with inertia, J , and no friciton, the dynamics are

$$
T=J s^{2} \theta
$$

If you apply a proportional-derivative feedback control law

$$
T=P\left(\theta_{r}-\theta\right)-D s \theta
$$

then the dynamics become

$$
P \theta_{r}=J s^{2} \theta+D s \theta+P \theta
$$

or

$$
\theta=\left(\frac{P}{J s^{2}+D s+P}\right) \theta_{r}
$$

D and P are chosen to place the poles of the closed-loop system.

Assume $\mathrm{J}=5$ (worst case for mass 1 ). To place the closed-loop poles at

$$
s=-4 \pm j 4
$$

you get

$$
\begin{aligned}
& J s^{2}+D s+P=5\left(s^{2}+8 s+32\right) \\
& D=40 \\
& P=160
\end{aligned}
$$

```
Assume \(\mathrm{J}=1\) (worse case for mass 2)
    \(J s^{2}+D s+P=1\left(s^{2}+2 s+2\right)\)
    D \(=2\)
    \(\mathrm{P}=2\)
```

Applying this feedback control law

```
for i=1:length(Qr)
```

    \(\mathrm{T} 1=160 *(\operatorname{Qr}(1, \mathrm{i})-\mathrm{Q}(1))+40 *(0-\mathrm{dQ}(1))\);
    \(T 2=32^{*}(\operatorname{Qr}(2, i)-Q(2))+8^{*}(0-d Q(2))\);
    T = [T1; T2];
    ddQ = TwoLinkDynamics(Q, dQ, T);
    \(d Q=d Q+d d Q\) * dt;
    \(\mathrm{Q}=\mathrm{Q}+\mathrm{dQ} \mathrm{A}^{\mathrm{d}}\);
    \(\mathrm{t}=\mathrm{t}+\mathrm{dt}\);
    \% rest of code ...
    

Tracking of the RR robot for a PD controller

One of the reasons the robot is not tracking the desired angle well is gravity is pulling down.

## PD Control with Gravity Compensation (FeedForward Control)

If you solve the previous dynamics for torque, you get:

$$
\left[\begin{array}{l}
\mathrm{T}_{1} \\
\mathrm{~T}_{2}
\end{array}\right]=\left[\begin{array}{cc}
\left(4+2 \mathrm{c}_{2}\right) & \left(1+\mathrm{c}_{2}\right) \\
\left(1+\mathrm{c}_{2}\right) & 1
\end{array}\right]\left[\begin{array}{l}
\ddot{\theta}_{1} \\
\ddot{\theta}_{2}
\end{array}\right]-\left[\begin{array}{c}
2 \mathrm{~s}_{2} \dot{\theta}_{1} \dot{\theta}_{2}+\mathrm{s}_{2} \dot{\theta}_{2}^{2} \\
-\mathrm{s}_{2} \dot{\theta}_{1}^{2}
\end{array}\right]-\mathrm{g}\left[\begin{array}{c}
3 \mathrm{c}_{1}+\mathrm{c}_{12} \\
\mathrm{c}_{12}
\end{array}\right]
$$

To compensate for gravity, add a term

$$
\left[\begin{array}{l}
\mathrm{T}_{1} \\
\mathrm{~T}_{2}
\end{array}\right]=\mathrm{T}_{\mathrm{PD}}-\mathrm{g}\left[\begin{array}{c}
3 \mathrm{c}_{1}+\mathrm{C}_{12} \\
\mathrm{C}_{12}
\end{array}\right]
$$

Note that you can do this offline: once you compute the desired tip positions and angles, you can compute the torque due to gravity. This speeds up the compuations while running.


## PD Control with Gravity and Coriolis Force Compensation (Feedforward Control)

Similarly, if you add in the coriolis forces as well you get slightly better tracking


## Velocity Feedfoward Control:

Once you cancel the gravity and coriolis terms, the dynamics become

$$
\theta=\left(\frac{P}{J s^{2}+D s+P}\right) \theta_{r}
$$

Ideally, the transfer funciton should be 1 (meaning the angle exactly matches the desired angle). If you add a derivative term

$$
\mathrm{T}=\mathrm{T}_{\mathrm{PD}}-\mathrm{T}_{\mathrm{g}}+\mathrm{DS} \theta_{\mathrm{r}}
$$

you get

$$
\theta=\left(\frac{D s+P}{J s^{2}+D s+P}\right) \theta_{r}
$$

which is closed to one (meaning better tracking). To do this, you need to

- Take the derivative of the deisred angles, and
- Bias the torque by D times this derivative

In Matlab:

```
% Velocity - right after computing the desired angles
dQr1 = Derivative(Qr(1,:));
dQr2 = Derivative(Qr(2,:));
dQr = [dQr1 ; dQr2];
for i=1:length(Qr)
    T1 = 160*(Qr(1,i) - Q(1)) + 40*(dQr(1,i) - dQ(1));
    T2 = 32*(Qr(2,i) - Q(2)) + 8*(dQr(2,i) - dQ(2));
    T = [T1; T2];
    % plus gravity
    T = T - G(:,i);
    % plus coriolis
    T = T - C(:,i);
```



## Accelearation Feedfoward Control:

Finally, if you also bias the torque by the acceleration term:

$$
\left[\begin{array}{l}
\mathrm{T}_{1} \\
\mathrm{~T}_{2}
\end{array}\right]=\left[\begin{array}{cc}
\left(4+2 \mathrm{C}_{2}\right) & \left(1+\mathrm{c}_{2}\right) \\
\left(1+\mathrm{C}_{2}\right) & 1
\end{array}\right]\left[\begin{array}{l}
\ddot{\theta}_{1} \\
\ddot{\theta}_{2}
\end{array}\right]
$$

you get a transfer function of

$$
\theta=\left(\frac{J s^{2}+D s+P}{J s^{2}+D s+P}\right) \theta_{r}
$$

```
% plus gravity
T = T - G(:,i);
% plus derivative
T = T + diag([40, 8]) *dQr(:,i);
% plus coriolis
T = T - C(:,i);
% plus acceleration
c2 = cos(Q(2));
T = T + [4+2*c2, 1+c2 ; 1+c2, 1]*ddQr(:,i);
```



Actual \& Dsired Tip Position for PD, Gravity, Coriolis, Derivative, and Inertia Compensation

```
% RR_Control.txt
% Position control of a RR robot
% similar to a RRR robot with Q1 = 0, meaning Y=0
%
% Define a square to trace
disp('Defining Path to Follow');
P1 = [0.5, 0]';
P2 = [1.5, 0]';
P3 = [1.5,-1]';
P4 = [0.5,-1]';
P5 = P1;
disp('Calculating tip positions');
% Determine the tip positions every 10ms
[A,T1] = MoveTo(P1,P2,2);
[A,T2] = MoveTo(P2,P3,2);
[A,T3] = MoveTo(P3,P4,2);
[A,T4] = MoveTo(P4,P5,2);
TIP = [T1,T2,T3,T4];
```

disp('Calculating joint angles');
\% Determie the joint angles every 10ms
Qr = [];
for i=1:length(TIP)
$\mathrm{q}=\operatorname{InverseRR(TIP(:,i));~}$
Qr = [Qr, q];
end
$\mathrm{c} 1=\cos (\operatorname{Qr}(1,:))$;
s1 $=\sin (\operatorname{Qr}(1,:))$;
$\mathrm{c} 2=\cos (\operatorname{Qr}(2,:))$;
$\mathrm{s} 2=\sin (\operatorname{Qr}(2,:))$;
$\operatorname{c12}=\cos (\operatorname{Qr}(1,:)+\operatorname{Qr}(2,:))$;
$\mathrm{s} 12=\sin (\operatorname{Qr}(1,:)+\operatorname{Qr}(2,:))$;
disp('Calulating gravity matrix');
\% gravity
$\mathrm{g}=9.8$;
$\mathrm{G}=\mathrm{g}^{*}\left[3^{*} \mathrm{c} 1+\mathrm{c} 12\right.$;
c12 ];
disp('Calulating gravity torques');
\% Velocity
dQr1 = Derivative(Qr(1,:));
dQr2 = Derivative(Qr(2,:));
$\mathrm{dQr}=$ [dQr1 ; dQr2];
disp('Calulating coriolis torques');
\% Coriolis Forces
$\mathrm{C}=\left[2^{*} \mathrm{~s} 2 . * \mathrm{dQr} 1 .{ }^{*} \mathrm{dQr} 2+\mathrm{s} 2 . * \mathrm{dQr} 2 . * \mathrm{dQr} 2\right.$;
-s2.*dQr1.*dQr1 ];
disp('Calulating inertia torques');
\% Acceleration
ddQr1 = Derivative(dQr(1,:));
ddQr2 = Derivative(dQr(2,:));
ddQr = [ddQr1 ; ddQr2];
\% Inertia
M = [];
for $i=1: l e n g t h(Q r)$
$M=\left[M,\left[4+2^{*} c 2(i), 1+c 2(i) ; 1+c 2(i), 1\right] * d d Q r\right] ;$
end

```
Q = Qr(:,1);
dQ = [0; 0];
T = [0; 0];
t = 0;
dt = 0.01;
TIP = [];
TIPr = [];
disp('Tracing out a Square');
for i=1:length(Qr)
    T1 = 160*(Qr(1,i) - Q(1)) + 40*(dQr(1,i) - dQ(1));
    T2 = 32*(Qr(2,i) - Q(2)) + 8*(dQr(2,i) - dQ(2));
    T = [T1; T2];
        % plus gravity
    T = T - G(:,i);
    % plus derivative
    % (already in the T1 and T2 equations )
    % plus coriolis
    T = T - C(:,i);
    % plus acceleration
    c2 = cos(Q(2));
    T = T + [4+2*c2, 1+c2 ; 1+c2, 1]*ddQr(:,i);
    ddQ = TwoLinkDynamics(Q, dQ, T);
    dQ = dQ + ddQ * dt;
    Q = Q + dQ*dt;
    t = t + dt;
% Robot
    x0 = 0;
    y0 = 0;
    x1 = cos(Q(1));
    y1 = sin(Q(1));
    x2 = x1 + cos(Q(1) + Q(2));
    y2 = y1 + sin(Q(1) + Q(2));
    TIP = [TIP, [x2 ; y2]];
    % Reference Point
    xr0 = 0;
    yr0 = 0;
    xr1 = cos(Qr(1,i));
    yr1 = sin(Qr(1,i));
    xr2 = xr1 + cos(Qr(1,i) + Qr(2,i));
    yr2 = yr1 + sin(Qr(1,i) + Qr(2,i));
    TIPr = [TIPr, [xr2 ; yr2]];
    clf;
    plot([-0.5,2],[-0.5,2],'x');
    hold on;
    plot([-0.5,2],[0,0], 'r');
    plot([0,0],[-0.5,2]', 'r')';
    plot([x0, x1, x2], -[y0, y1, y2], 'b.-', [xr0, xr1, xr2], -[yr0, yr1, yr2], 'c.-');
plot(TIPr(1,:),-TIPr(2,:),'g', TIP(1,:),-TIP(2,:),'m');
    pause(0.01);
end
```

